

# State-feedback $H_\infty$ control of nonlinear singularly perturbed systems

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## SUMMARY

We study the  $H_\infty$  control problem for an affine singularly perturbed system, which is nonlinear in the state variables. Under suitable assumptions on the linearized problem, we construct  $\varepsilon$ -independent composite and linear controllers that solve the local  $H_\infty$  control problem for the full-order system for all small enough  $\varepsilon$ . These controllers solve also the corresponding problem for the descriptor system. The ‘central’ nonlinear controller can be approximated in the form of expansions in the powers of  $\varepsilon$ . An illustrative example shows that the higher-order approximate controller achieves the better performance, while the composite (zero-order approximate) controller leads to the better performance than the linear one. Copyright © 2001 John Wiley & Sons, Ltd.

KEY WORDS:  $H_\infty$  control; nonlinear systems; singular perturbations; descriptor systems

## 1. INTRODUCTION

$H_\infty$ -control of a class of singularly perturbed system being nonlinear only on the slow variable have been studied in References [1–3]. In Reference [1] a composite  $\varepsilon$ -independent controller has been designed. In Reference [2] it has been shown that any  $\varepsilon$ -independent  $H_\infty$  controller of the linearized singularly perturbed system is a local  $H_\infty$  controller for nonlinear problem. In Reference [3] a high-order approximate controller has been constructed in the form of expansions in the powers of  $\varepsilon$ .

In the present note, we consider a general singularly perturbed system, being affine in the control and nonlinear in both, the slow and the fast variables. We generalize results of References [4, 5] obtained for the case of optimal control problem of such systems to the  $H_\infty$  control: we construct an  $\varepsilon$ -independent composite controller and a high-order approximate one by expanding in the powers of  $\varepsilon$  the ‘central’ controller, that solves the problem for each  $\varepsilon$ . Assuming that the

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corresponding linearized  $H_\infty$  control problem is solvable we show that

- (i) the composite controller is  $O(\varepsilon)$ -close to the 'central' one and solves the local  $H_\infty$  control problem for the singularly perturbed system for all small enough  $\varepsilon > 0$ ;
- (ii) the composite controller solves the local  $H_\infty$  control problem for the corresponding descriptor system;
- (iii) the truncated expansion approximates the 'central' controller and solves the local  $H_\infty$  control problem.

Proofs of the theorems are given in the appendix.

## 2. PROBLEM FORMULATION

Consider the system

$$\dot{x}_1 = F_1(x_1, x_2) + B_1(x_1, x_2)u + D_1(x_1, x_2)w \quad (1a)$$

$$\varepsilon \dot{x}_2 = F_2(x_1, x_2) + B_2(x_1, x_2)u + D_2(x_1, x_2)w \quad (1b)$$

$$z = \text{col} \{k(x_1, x_2), u\} \quad (1c)$$

where  $x_1(t) \in \mathbf{R}^{n_1}$  and  $x_2(t) \in \mathbf{R}^{n_2}$  are the state vectors,  $x = \text{col} \{x_1, x_2\}$ ,  $u(t) \in \mathbf{R}^m$  is the control input,  $w \in \mathbf{R}^q$  is the disturbance and  $z \in \mathbf{R}^s$  is the output to be controlled. The functions  $F_i$ ,  $B_i$ ,  $D_i$  and  $k$  are differentiable with respect to  $x$  a sufficient number of times. We assume also that  $F_i(0, 0) = 0$  and  $k(0, 0) = 0$ .

Unlike Reference [1] we consider a non-standard singularly perturbed problem in the sense that we do not require the solvability with respect to  $x_2$  of the algebraic equation

$$F_2(x_1, x_2) + B_2(x_1, x_2)u + D_2(x_1, x_2)w = 0$$

For more information on non-standard singularly perturbed system we refer to Reference [5] and example therein, where the above algebraic equation has the form  $x_1 + u = 0$ .

Denote by  $|\cdot|$  the Euclidean norm of a vector. Let  $\gamma$  be a fixed positive constant. Then, the nonlinear  $H_\infty$  control problem (for performance level  $\gamma$ ) is to find a nonlinear state-feedback

$$u = \beta(x), \quad \beta(0) = 0 \quad (2)$$

such that the closed-loop system of (1) and (2) has a  $L_2$ -gain less than or equal to  $\gamma$  (see Reference [6]). It means that the following inequality holds:

$$\int_0^\tau |z(t)|^2 dt \leq \gamma^2 \int_0^\tau |w(t)|^2 dt \quad (3)$$

for all  $w \in L_2[0, \tau]$  and all  $\tau \geq 0$ , where  $z$  denotes the response of the closed-loop system of (1) and (2) for  $w \in L_2[0, \tau]$  and the initial condition  $x(0) = 0$  (see References [6, 7]). The  $H_\infty$  control problem is solvable on  $\Omega \subset \mathbf{R}^{n_1} \times \mathbf{R}^{n_2}$  containing 0 as an interior point if (3) holds for every  $\tau \geq 0$  and for every  $w \in L_2[0, \tau]$  for which the state trajectory of the closed-loop system (1) and (2) starting from 0 remains in  $\Omega$  for all  $t \in [0, \tau]$ .

Consider the Hamiltonian function

$$\begin{aligned} \mathcal{H}(x_1, x_2, p_1, p_2) = & p_1' F_1(x_1, x_2) + p_2' F_2(x_1, x_2) \\ & - \frac{1}{2} (p_1' p_2') \begin{pmatrix} S_{11}(x) & S_{12}(x) \\ S_{21}(x) & S_{22}(x) \end{pmatrix} \begin{pmatrix} p_1 \\ p_2 \end{pmatrix} + \frac{1}{2} k'(x_1, x_2) k(x_1, x_2) \end{aligned} \quad (4)$$

where prime denotes the transposition of a matrix,  $p_1$  and  $\varepsilon p_2$  play the role of the co-state variables and  $S_{ij} = B_i B_j' - 1/\gamma^2 D_i D_j'$ . The corresponding Hamiltonian system has the form

$$\dot{x}_1 = f_1(x_1, p_1, x_2, p_2) \quad (5a)$$

$$\dot{p}_1 = f_2(x_1, p_1, x_2, p_2) \quad (5b)$$

$$\varepsilon \dot{x}_2 = f_3(x_1, p_1, x_2, p_2) \quad (5c)$$

$$\varepsilon \dot{p}_2 = f_4(x_1, p_1, x_2, p_2) \quad (5d)$$

where  $f_1 = (\partial \mathcal{H} / \partial p_1)'$ ,  $f_2 = -(\partial \mathcal{H} / \partial x_1)'$ ,  $f_3 = (\partial \mathcal{H} / \partial p_2)'$ ,  $f_4 = -(\partial \mathcal{H} / \partial x_2)'$ .

For each  $\varepsilon > 0$  the problem is solvable on  $\Omega \subset \mathbf{R}^{n_1} \times \mathbf{R}^{n_2}$  if there exists a  $C^2$  non-negative solution  $V: \Omega \rightarrow \mathbf{R}$  to the Hamilton–Jacobi (HJ) partial differential equation

$$\begin{aligned} & V_{x_1} F_1(x_1, x_2) + \varepsilon^{-1} V_{x_2} F_2(x_1, x_2) \\ & - \frac{1}{2} (V_{x_1} \varepsilon^{-1} V_{x_2}) \begin{pmatrix} S_{11}(x) & S_{12}(x) \\ S_{21}(x) & S_{22}(x) \end{pmatrix} \begin{pmatrix} V_{x_1}' \\ \varepsilon^{-1} V_{x_2}' \end{pmatrix} + \frac{1}{2} k'(x_1, x_2) k(x_1, x_2), \quad V(0) = 0 \end{aligned} \quad (6)$$

with the property that the system

$$\dot{x}_1 = f_1(x_1, V_{x_1}', x_2, \varepsilon^{-1} V_{x_2}'), \quad \varepsilon \dot{x}_2 = f_3(x_1, V_{x_1}', x_2, \varepsilon^{-1} V_{x_2}') \quad (7)$$

is asymptotically stable (see References [6, 7]), where  $V_x = (V_{x_1}, V_{x_2})$  denotes the Jacobian matrix of  $V$ . The latter is equivalent to the existence of the invariant manifold of (5)  $p_1 = V_{x_1}'$ ,  $p_2 = \varepsilon^{-1} V_{x_2}'$ , with asymptotically stable flow, such that  $V \geq 0$ ,  $V(0) = 0$  (that implies  $V_x(0) = 0$ ). The controller that solves the problem is then given by

$$u = -[B_1', \varepsilon^{-1} B_2'] V_x' \quad (8)$$

Similarly to the linear case, the latter will be denoted as the ‘central’ controller.

Note that the ‘central’ controller of (8) is found by solving high-order  $\varepsilon$ -dependent HJ partial differential equation (6). We shall construct  $H_\infty$  controllers by solving the simplified  $\varepsilon$ -independent reduced-order partial differential and algebraic equations.

### 3. MAIN RESULTS

#### 3.1. $H_\infty$ composite controller

Composite controller will be constructed similar to the one in the optimal control case (see Reference [5]). Consider the linearization of (1) at  $x = 0$ :

$$\begin{aligned} \dot{x}_1 = & A_{11} x_1 + A_{12} x_2 + B_{10} u + D_{10} w, \quad \varepsilon \dot{x}_2 = A_{21} x_1 + A_{22} x_2 + B_{20} u + D_{20} w \\ z = & \text{col} \{C_1 x_1 + C_2 x_2, u\} \end{aligned} \quad (9)$$

where  $A_{ij} = (\partial f_i / \partial x_j)(0, 0)$ ,  $B_{i0} = B_i(0, 0)$ ,  $D_{i0} = D_i(0, 0)$ ,  $C_i = (\partial k / \partial x_i)(0, 0)$ ,  $i = 1, 2$ ;  $j = 1, 2$ . Hamiltonian system that corresponds to (9) can be written in the form

$$\begin{bmatrix} \dot{x}_1 \\ \dot{p}_1 \\ \dot{x}_2 \\ \dot{p}_2 \end{bmatrix} = \text{Ham} \begin{bmatrix} x_1 \\ p_1 \\ x_2 \\ p_2 \end{bmatrix} \tag{10a}$$

$$\text{Ham} = \begin{bmatrix} T_{11} & T_{12} \\ \varepsilon^{-1}T_{21} & \varepsilon^{-1}T_{22} \end{bmatrix} \tag{10b}$$

$$T_{ij} = \begin{bmatrix} A_{ij} & -S_{ij}(0) \\ -C'_i C_j & -A'_{ji} \end{bmatrix} \tag{10c}$$

To guarantee that for all small  $\varepsilon$  this linear  $H_\infty$  control problem is solvable we assume:

A1

For a given  $\gamma$  a fast Riccati equation

$$A'_{22}X_f + X_f A_{22} + C'_2 C_2 - X_f S_{22}(0) X_f = 0 \tag{11}$$

has a solution  $X_f = X'_f \geq 0$ , such that the matrix  $\Lambda_f = A_{22} - S_{22} X_f$  is Hurwitz.

A2

For a given  $\gamma$  a slow Riccati equation

$$X_0 A_0 + A'_0 X_0 - X_0 S_0 X_0 + Q_0 = 0 \tag{12}$$

where

$$\begin{bmatrix} A_0 & -S_0 \\ -Q_0 & -A'_0 \end{bmatrix} = T_{11} - T_{12} T_{22}^{-1} T_{21} \tag{13}$$

has a solution  $X_0 = X'_0 \geq 0$  such that the matrix  $\Lambda_s = A_0 - S_0 X_0$  is Hurwitz.

Note that under assumptions of stabilizability–detectability and absence of invariant zeros on the imaginary axis of Reference [8] assumptions A1 and A2 are necessary and sufficient for solvability of the linear  $H_\infty$  control problem for all small enough  $\varepsilon$ . It is known (see Reference [8]) that under A1 and A2 for all small enough  $\varepsilon$  the linear controller

$$u_l = -B'_{10} X_0 x_1 - B'_{20} (X_c x_1 + X_f x_2), \quad X_c = [X_f, -I] T_{22}^{-1} T_{21} \begin{bmatrix} I \\ X_0 \end{bmatrix} \tag{14}$$

solves the linear  $H_\infty$  control problem. Therefore, for each small  $\varepsilon$ , the  $H_\infty$  control problem is solvable on a small enough neighbourhood of  $\mathbf{R}^{n_1} \times \mathbf{R}^{n_2}$  containing 0 (see Reference [6]). We shall show that there exists an  $\varepsilon$ -independent neighbourhood that is appropriate for all small enough  $\varepsilon$ .

Under A1 the Hamiltonian matrix  $T_{22}$  has  $n_2$  eigenvalues with negative real parts and  $n_2$  with positive ones. Under A1 and A2 the Hamiltonian matrix  $T_0 = T_{11} - T_{12} T_{22}^{-1} T_{21}$ , has  $n_1$  eigenvalues with negative real parts and  $n_1$  with positive ones. Then by implicit function theorem

in a small enough neighbourhood of  $\mathbf{R}^{n_1} \times \mathbf{R}^{n_2}$  containing 0 the system of equations

$$f_3(x_1, p_1, x_2, p_2) = 0, \quad f_4(x_1, p_1, x_2, p_2) = 0$$

has an isolated solution

$$x_2 = \phi(x_1, p_1), \quad p_2 = \psi(x_1, p_1) \quad (15)$$

Consider the *reduced* Hamiltonian system

$$\dot{x}_1 = f_1(x_1, p_1, \phi(x_1, p_1), \psi(x_1, p_1)) \quad (16a)$$

$$\dot{p}_1 = f_2(x_1, p_1, \phi(x_1, p_1), \psi(x_1, p_1)) \quad (16b)$$

This system results after substituting (15) into (5a) and (5b). From A2 and the theory of nonlinear differential equations (see e.g. Reference [9]) it follows that this system has a stable manifold

$$p_1 = N_0(x_1), \quad N_0(x_1) = X_0 x_1 + O(|x_1|^2) \quad (17)$$

with asymptotically stable flow

$$\dot{x}_1 = f_1(x_1, N_0(x_1), \phi(x_1, N_0(x_1)), \psi(x_1, N_0(x_1))) \quad (18)$$

for  $x_1$  from small enough neighbourhood of 0. Function  $N_0 = N_0(x_1)$  satisfies the *slow*  $\varepsilon$ -independent partial differential equation (PDE)

$$\frac{\partial N_0}{\partial x_1} f_1(x_1, N_0, \phi(x_1, N_0), \psi(x_1, N_0)) = f_2(x_1, N_0, \phi(x_1, N_0), \psi(x_1, N_0)) \quad (19)$$

Approximate solution of the slow PDE may be obtained by the power-series method as given in Reference [10] (see also Reference [6] and references therein). Due to this method  $N_0$  can be approximately found in the form of expansion in the powers of  $x_1$ :

$$N_0(x_1) = X_0 x_1 + N^{(2)}(x_1) + N^{(3)}(x_1) + \dots \quad (20)$$

with  $N^{(i)}$  denoting the  $i$ th-order terms of  $N_0(x_1)$ . Substitution of (20) into (19) and equating of terms of the same order lead to algebraic equations with respect to  $N^{(i)}$ . From the latter equations  $N^{(i)}$  can be computed inductively via  $X_0, \dots, N^{(i-1)}$ .

For each  $x_1$  such that (17) exists consider the 'fast' system

$$\dot{x}_2 = \bar{f}_3(x_1, x_2, p_2), \quad \dot{p}_2 = \bar{f}_4(x_1, x_2, p_2) \quad (21)$$

where

$$\bar{f}_i = f_i(x_1, N_0, x_2 + \phi(x_1, N_0), p_2 + \psi(x_1, N_0)), \quad i = 3, 4$$

For each  $x_1$  (21) has a stable manifold  $p_2 = M_0(x_1, x_2)$  with asymptotically stable flow

$$\dot{x}_2 = \bar{f}_3(x_1, x_2, M_0(x_1, x_2))$$

where  $x_1$  and  $x_2$  from small enough neighbourhood  $\Omega$  of  $\mathbf{R}^{n_1} \times \mathbf{R}^{n_2}$  containing 0. Function

$$M_0 = M_0(x_1, x_2) = X_f x_2 + O((|x_1| + |x_2|)|x_2|) \quad (22)$$

satisfies the *fast*  $\varepsilon$ -independent PDE

$$\frac{\partial M_0}{\partial x_2} \bar{f}_3(x_1, x_2, M_0) = \bar{f}_4(x_1, x_2, M_0) \tag{23}$$

Similarly to  $N_0$ , function  $M_0$  can be found in the form of expansion in the powers of  $x_2$ :

$$M_0(x_1, x_2) = X_f x_2 + M^{(2)}(x_1, x_2) + M^{(3)}(x_1, x_2) + \dots$$

with  $M^{(i)}(x_1, x_2)$  denoting the  $i$ th-order terms with respect to  $x_2$  and depending on the parameter  $x_1$ .

Define the *composite* controller as follows:

$$u_0(x) = -B_1' N_0(x_1) - B_2' [\psi(x_1, N_0(x_1)) + M_0[x_1, x_2 - \phi(x_1, N_0(x_1))]] \tag{24}$$

From (14), (17) and (22) it follows that

$$u_0 = u_t + O(|x_1|^2 + |x_2|^2) \tag{25}$$

Both  $\varepsilon$ -independent controllers, the composite (24) and the linear (14), solve  $H_\infty$  control problem on some neighbourhood for all small enough  $\varepsilon$ :

*Theorem 3.1*

Under A1 and A2 there exist  $m_1 > 0, m_2 > 0$  and  $\varepsilon_0 > 0$  such that for all  $\varepsilon \in (0, \varepsilon_0]$  the following holds:

- (i) There exists a  $C^2$  function  $V : \Omega_{m_1} \times \Omega_{m_2} \rightarrow [0, \infty)$ , satisfying the HJ equation (6). The solution to HJ equation and the ‘central’ controller have the following approximations:

$$V(x_1, x_2) = V_0(x_1) + O(\varepsilon), \quad u(x) = u_0(x) + O(\varepsilon) \tag{26}$$

where  $u_0$  is given by (24) and  $\partial V_0 / \partial x_1 = N_0'(x_1)$ .

- (ii)  $H_\infty$  control problem is solvable on  $\Omega_{m_1} \times \Omega_{m_2}$  by the composite controller of (24).
- (iii)  $H_\infty$  control problem is solvable on  $\Omega_{m_1} \times \Omega_{m_2}$  by the linear controller of (14).

*Remark 3.1*

Example in Reference [3] and the one below show that the composite controller leads to the better performance than the linear controller.

*3.2.  $H_\infty$  control of nonlinear descriptor system*

In this subsection, we show that similarly to the linear case (see Reference [8]), the composite controller solves  $H_\infty$  control problem for the corresponding descriptor system

$$E\dot{x} = F(x) + B(x)u + D(x)w, \quad z = \text{col}\{k(x), u\} \tag{27}$$

where  $k(x) = k(x_1, x_2)$  and

$$E = \begin{bmatrix} I_{n_1} & 0 \\ 0 & 0 \end{bmatrix}, \quad F = \begin{bmatrix} F_1(x_1, x_2) \\ F_2(x_1, x_2) \end{bmatrix}, \quad B = \begin{bmatrix} B_1(x_1, x_2) \\ B_2(x_1, x_2) \end{bmatrix}, \quad D = \begin{bmatrix} D_1(x_1, x_2) \\ D_2(x_1, x_2) \end{bmatrix}$$

Unlike the non-descriptor case, the initial condition for (27) is defined only for the slow variable  $x_1$ . We restrict ourselves to *admissible* controllers of form (8) which guarantee a unique solution to the closed-loop system (27) and (8) for any small enough initial condition  $Ex(0)$  and for any square integrable function  $w(\cdot)$  from small enough neighbourhood of 0 in  $R^q$ . An admissible controller solves local  $H_\infty$  control problem for (27) on  $\Omega \subset R^{m_1} \times R^{m_2}$  containing 0 as an interior point if (3) holds for every  $\tau \geq 0$  and for every square integrable  $w \in L_2[0, \tau]$  for which the state trajectory of the closed-loop system (27) and (8) starting from  $Ex(0) = 0$  is uniquely defined and remains in  $\Omega$  for all  $t \in [0, \tau]$ .

*Theorem 3.2*

Under A1 and A2 the following holds:

- (i) Let there exists a twice continuously differentiable function  $V_d: \Omega_{m_1} \times \{0\} \rightarrow R$  such that  $V_d(Ex) \geq 0$ ,

$$\frac{\partial V_d(Ex)}{\partial x} = W(x)E \quad (28)$$

$$2W(x)F(x) - W(x)S(x)W'(x) + k'(x)k(x) = 0, \quad S = BB' - \gamma^{-2}DD' \quad (29)$$

with the property that  $\tilde{f}_{x_2}(0)$  and  $\tilde{F}_{x_2}(0)$  are non-singular, where  $\tilde{f} = F_2 - B_2B_2'W'$ ,  $\tilde{F} = F_2 - SW'$ , and that the systems

$$E\dot{x} = F(x) - B(x)B'(x)W'(x), \quad E\dot{x} = F(x) - S(x)W'(x) \quad (30)$$

are asymptotically stable. Then the controller

$$u_d(x) = -B'(x)W'(x) \quad (31)$$

solves the local  $H_\infty$  control problem for the descriptor system (27).

- (ii) The composite controller (24) solves the local  $H_\infty$  control problem for (27).  
 (iii) The linear controller (9) solves the local  $H_\infty$  control problem for (27).

*3.3. High-order approximate controller*

An asymptotic approximation to the controller (8)

$$u(x) = u_q(x) + O(\varepsilon^{q+1}), \quad u_q(x) = \sum_{i=0}^q \varepsilon^i u^{(i)}(x) \quad (32)$$

can be found similarly to Reference [4] by expanding the invariant manifolds into the powers of  $\varepsilon$ . The controller  $u_q$  solves local  $H_\infty$  control problem:

*Theorem 3.3*

Given  $\gamma > 0$ , under A1 and A2 there exist  $m_1, m_2, \varepsilon_1$  such that for all  $\varepsilon \in (0, \varepsilon_1]$  the following holds on  $\Omega_{m_1} \times \Omega_{m_2}$ :

- (i) The 'central' controller exists and can be approximated by (32), where all functions are continuously differentiable in  $x$  and approximation is uniform on  $x$  and  $\varepsilon$ .  
 (ii)  $H_\infty$  control problem is solvable on  $\Omega_{m_1} \times \Omega_{m_2}$  by the controller  $u_q$ .

Examples in Reference [3] and the one below show that the higher-order terms in (32) lead to improved performance.

### 3.4. Example

Consider the systems

$$\dot{x}_1 = -\tan x_2 + 2u + w, \quad \varepsilon \dot{x}_2 = \tan x_2 - u, \quad z = (x_1 \ u)' \quad (33)$$

Here (11) has a stabilizing solution  $X_f = 2$ . We obtain the following Hamiltonian function:

$$\mathcal{H} = -p_1 \tan x_2 + p_2 \tan x_2 + 1/2(1/\gamma^2 - 4)p_1^2 + 2p_1 p_2 - 1/2p_2^2 + 1/2x_1^2$$

and the corresponding Hamiltonian system

$$\begin{aligned} \dot{x}_1 &= -\tan x_2 + (1/\gamma^2 - 4)p_1 + 2p_2, & \dot{p}_1 &= -x_1 \\ \varepsilon \dot{x}_2 &= \tan x_2 + 2p_1 - p_2, & \varepsilon \dot{p}_2 &= \cos^{-2} x_2 (p_1 - p_2) \end{aligned}$$

We find

$$\phi = -\arctan p_1, \quad \psi = p_1, \quad N_0 = Kx_1, \quad M_0 = 2 \tan[x_2 - \arctan(Kx_1)] + 2Kx_1$$

where  $K = (1 - 1/\gamma^2)^{-0.5}$ , and A2 is satisfied for  $\gamma > 1$ . The linear (14) and the composite (24) controllers have the following form:

$$u_l = Kx_1 + 2x_2, \quad u_0 = Kx_1 + 2 \tan x_2 \quad (34)$$

By algorithm of Reference [4] we find the first-order approximate controller  $u_1$ :

$$u_1 = u_0 + 3\varepsilon K(x_2 + \arctan(Kx_1)) + \frac{\varepsilon x_1}{1 + K^2 x_1^2} - 4\varepsilon \frac{x_1 \sec^2 x_2}{(1 + K^2 x_1^2)^2} + \varepsilon l, \quad l = O(|x_2 + \arctan(Kx_1)|^2)$$

We made some simulations of the behaviour of (33) under  $u_l$ ,  $u_0$  and  $u_1$  (with  $l = 0$ ) and constant and sinusoidal disturbance functions. Choosing  $\gamma = 1.1 > 1$  we found  $K = 2.4004$ . Thus, for  $w(t) = 0.5 \sin 3t$  the values of the functional cost

$$J = \int_0^t [x_1^2(s) + u^2(s) - \gamma^2 w^2(s)] ds$$

under all these controllers are negative for the following values of  $\varepsilon < 0.08$ :  $\varepsilon = 0.07$ ,  $0.001$  and  $0$ . Therefore, under this particular disturbance input all the controllers achieve the performance bound of  $\gamma = 1.1$ .

We include in Figure 1 plots of the functional cost for  $w(t) = 0.5 \sin 3t$ ,  $\varepsilon = 0.08$  and  $\varepsilon = 0.09$ , where ‘.’ is the plot under  $u = u_l$ , ‘- -’ is the plot under  $u = u_0$  and ‘-’ is the plot under  $u = u_1$ . For  $\varepsilon = 0.08$  functional costs under  $u_0$  and  $u_1$  are negative, while for  $u_l$  it becomes positive for  $t > 15$ . Hence, under this particular disturbance input the composite and the first-order controllers achieve the performance bound of  $\gamma = 1.1$ , whereas, the linear controller does not achieve this bound. For  $\varepsilon = 0.9$  only the first-order controller  $u_1$  leads to negative values of cost and, hence achieves the performance bound  $\gamma = 1.1$ . Therefore, the linear controller (14) is robust for  $0 \leq \varepsilon \leq 0.07$ , the composite controller (34) is robust for  $0 \leq \varepsilon \leq 0.08$  in the sense that they achieve  $\gamma = 1.1$  for  $w = 0.5 \sin 3t$ . For  $\varepsilon = 0.09$  only  $u_1$  achieves  $\gamma = 1.1$  for  $w = 0.5 \sin 3t$ . Thus the  $O(\varepsilon^2)$ -approximation to the ‘central’ controller (8) achieves the better performance bound than its



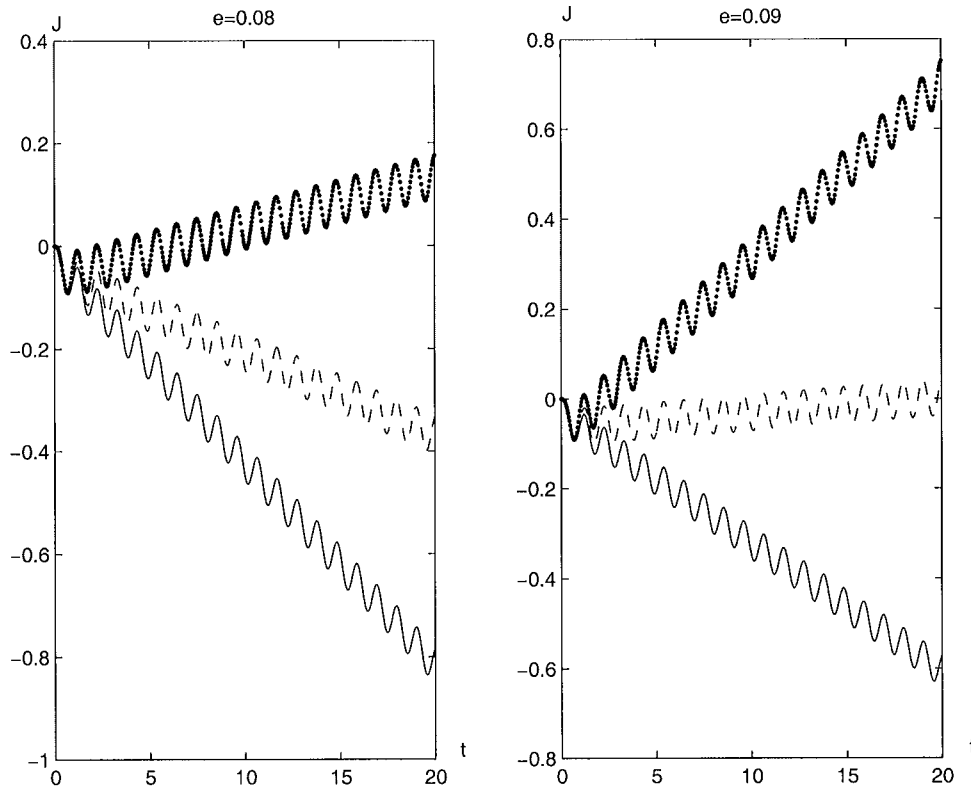


Figure 1. Functional costs for  $\gamma = 1.1$  and  $w = 0.5 \sin 3t$ : (· · · · ·)  $u = u_1$ ; (- - -)  $u = u_0$ ; (—)  $u = u_1$ .

$O(\varepsilon)$ -approximation, whereas, the composite controller leads to the better performance than the linear one.

#### 4. CONCLUSIONS

We have designed robust  $\varepsilon$ -independent  $H_\infty$  controllers for singularly perturbed systems that are nonlinear in both, the slow and the fast state variables. We have shown that these controllers achieve  $\gamma$  performance for all small enough  $\varepsilon$ . Moreover, they solve a local  $H_\infty$ -control problem for the corresponding descriptor system. We have shown that a higher-order accuracy controller improves the performance.

#### APPENDIX

*Proof of Theorem 3.1.* (i) The existence of  $C^2$  solution to (6) and (26) follows from Reference [4]. We shall show that  $V \geq 0$  by proving that the closed-loop system of (1) and (8) with  $w = 0$  is

asymptotically stable (see References [6, 7]). To prove the latter consider linearization of the closed-loop system in the 0:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} \tilde{A}_{11} & \tilde{A}_{22} \\ \varepsilon^{-1}\tilde{A}_{21} & \varepsilon^{-1}\tilde{A}_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} A_{11} & A_{22} \\ \varepsilon^{-1}A_{21} & \varepsilon^{-1}A_{22} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} B_{10} \\ \varepsilon^{-1}B_{20} \end{bmatrix} u_t \quad (A1)$$

Under A1 and A2 the fast matrix  $\tilde{A}_{22}$  and the reduced one  $\tilde{A}_{11} - \tilde{A}_{12}\tilde{A}_{22}^{-1}\tilde{A}_{21}$  are Hurwitz (see proof of Lemma 3.4 from Reference [11]). The system of (1) and (8) with  $w = 0$  is then asymptotically stable since its fast and reduced systems are stable (see e.g. Reference [12]).

(ii) Consider the closed-loop system of (1) and (24). We have to prove that the corresponding to this system HJ equation has a non-negative stabilizing solution. Due to (ii) of this theorem we have to verify that assumptions A1 and A2 are satisfied for the corresponding linearized problem

$$\dot{x}_1 = \tilde{A}_{11}x_1 + \tilde{A}_{12}x_2 + D_{10}w, \quad \varepsilon\dot{x}_2 = \tilde{A}_{21}x_1 + \tilde{A}_{22}x_2 + D_{20}w, \quad z = [\tilde{C}_1 \quad \tilde{C}_2]x \quad (A2)$$

where  $\tilde{C}_1 = [C_1, B'_{10}X_0 - B'_{20}X_c]$ ,  $\tilde{C}_2 = [C_2, -B'_{20}X_f]$ . Note that the latter system coincides with the closed-loop system of (9) and (14). Hamiltonian system that corresponds to (A2) has the form

$$\begin{bmatrix} \dot{x}_1 \\ \dot{p}_1 \\ \dot{x}_2 \\ \dot{p}_2 \end{bmatrix} = \tilde{\text{Ham}} \begin{bmatrix} x_1 \\ p_1 \\ x_2 \\ p_2 \end{bmatrix} \quad (A3)$$

where  $\tilde{\text{Ham}}$  is defined by (10) with all matrices taken with tilde and  $\tilde{S}_{ij} = -\gamma^{-2}D_iD'_j$ .

We observe that A1 and A2 means that the fast and the reduced systems corresponding to (A3) have stable manifolds. Set  $\varepsilon = 0$  and see that substitution of  $p_1 = X_0x_1$  and  $p_2 = X_cx_1 + X_fx_2$  leads (A3) to (10) with  $\varepsilon = 0$ . Therefore,  $p_2 = X_fx_2$  and  $p_1 = X_0x_1$  are the above-mentioned stable manifolds.

Proof of (iii) is similar to (ii).

*Proof of Theorem 3.2.* (i) Let  $x(t)$  satisfies (27) and initial condition  $Ex(0) = 0$ . Applying (28), (27) and (29) we find

$$\begin{aligned} 2 \frac{dV_d(Ex)}{dt} - \gamma^2 w'w + z'z &= 2W(x)(f(x) + B(x)u + D(x)w) - \gamma^2 w'w + k'k + u'u \\ &= (u' + W(x)B(x))(u + B'(x)W'(x)) - \gamma^2(w' - \gamma^{-2}W'(x)D'(x))(w - \gamma^{-2}D(x)W) \end{aligned} \quad (A4)$$

Substituting in (A4)  $u = u_d$  and integrating the resulting inequality on  $t$  from 0 to  $\tau$  (for any  $\tau > 0$ ) we find

$$2V_d(Ex(\tau)) - \gamma^2 \int_0^\tau |w(t)|^2 dt + \int_0^\tau |z(t)|^2 dt \leq 0$$

that implies (3). Due to non-singularity of  $\tilde{f}_{x_2}(0)$  and  $\tilde{F}_{x_2}(0)$  systems (30) have unique solution for small enough  $Ex(0)$  and the closed-loop system (27) and (31) has a unique solution for small enough  $Ex(0)$  and  $w(\cdot)$ . Hence, controller (31) is admissible.

(ii) Choosing  $V_d(Ex) = V_0(x_1)$ , where  $V_0$  satisfies (26), we see that

$$\frac{\partial V_d(Ex)}{\partial x} = W(x)E, \quad W(x) = [N'_0(x_1) \psi'(x_1, N_0(x_1)) + M'[x_1, x_2 - \phi(x_1, N_0(x_1))]]$$

Since by Theorem 3.1  $[V_{x_1} \ \varepsilon^{-1}V_{x_2}] = W + O(\varepsilon)$ , where  $V$  is solution to HJ equation (6), then  $W$  satisfies (29). Moreover, (31) coincides with (24) that together with item (i) of this theorem completes the proof. Proof of (iii) is similar to (ii) of Theorem 3.1.  $\square$

*Proof of Theorem 3.3.* Item (i) follows from Reference [4]. Proof of (ii) is similar to (ii) of Theorem 3.1.

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